

CHAPTER - IV

OXIDATION OF AZELAIC AMIDE.

In order to decide the suitable temperature, concentration of the ractants and concentration of the silver catalyst some preliminary experiments were carried out. At room temp., it was observed that the uncatalysed reaction is very slow. The reaction proceeds with a measurable velocity at 35°C.

Thus the reaction was first studied at 35°C using the concentrations of $K_2S_2O_6$ as 2.0 x 10⁻²M, Substrate as 5.0 x 10⁻²M.and 1.0 x10⁻³M as silver catalyst. The results of this kinetic run is recorded in Table B - 1.

١

CARR. BALASAHEB KHARDEKAR LIBRAND

TABLE B - 1

Time (min.)	C*	k₁×10³min⁻¹
0	9.44	-
20	8.95	2.606
40	8.50	2.595
60	8.08	2.579
80	7.68	2.566
100	7.31	2.554
130	6.78	2.538
160	6.30	2.525
200	5.71	2.508
240	5.18	2.496
300	4.48	2.481
360	3.87	2.470
 Mean kı× 10³ min ⁻¹	ar an tha the the the tee for the the tee for the for the for the for the for the for the	2.538

 $K_2S_2O_6 = 2.0 \times 10^{-2}M$, Amide = 5.0 × 10⁻² M, AgNO₃= 1.0 × 10⁻³M, Temp. = 35°C.

[C* denotes the volume of $Na_2S_2O_3(0.02 \text{ M})$ in ml. equivalent to unreacted $S_2O_8^{2-3}$]

From the results contained in Table B - 1, it indicates that there is a fair constancy in the first order rate constant values, suggesting that the overall order of reaction at these concentrations of the reactants is unity. The concentration of substrate was taken in excess and so the order is with respect to $S_2O_e^{2-}$.

To decide conclusively the order with respect to $S_2O_{\Theta}^{2-}$ and substrate, another kinetic run having equimoler concentrations (0.02M each) of the two reactants was studied. The results of these measurements are recorded in Table B-2.

K ₂ S ₂ O _e = Substrate = 2.0 ×10 ⁻² M, AgNO ₃ = 1.0×10 ⁻³ M, Temp. = 35°C.					
Time (min.)	C	k₁ x 10 [∞] min ⁻¹			
0	9.46	· 			
20	8.85	3.312			
40	8.28	3.299			
60	7.76	3.285			
80	7.28	3.272			
100	6.83	3.255			
130	6.20	3.243			
160	5.64	3.225			
200	4.97	3.212			
240	4.39	3.194			
300	3.64	3.180			
360	3.02	3.163			
Mean k1 ×10 ³ min ⁻¹ .	12 - 1414 4804 4414 4414 4414 4414 4414 4414	3.240			

Here again, it is seen that the first order rate constant slightly decrease with time, which most probable may be due to some inihibition as the reaction progresses. The nearly constant values of the rate constant suggest that the order with respect to substrate may be zero.

EFFECT OF K2S20 CONCENTRATION

Before studying the effect of $K_2S_2O_8$ conc. on the reaction rate, it is necessary to study the self decomposition of peroxydisulphate without the substrate and in the presence of silver catalyst. The results of these kinetic runs are recorded in Table B - 3.

TABLE 8 - 3

Subet	rate -	5.0 ×10	-≃M, Agl	NO ₃ = 1.0>	(10 ⁻³ M,	Temp.= 3	5°C.	
[K2S2	0]M	0.01		0.02		0.03		0.04
Time (min.) C	k₁x10 ³ min ^{−1}	с	k₁×10³ min ^{−1}	С	k₁×10³ min⁻¹	С	k₁ ×10 ³ min ⁻¹
0	4.94		9.44	-	14.75		19.55	
20	4.65	2.931	8.95	2.606	14.09	2.267	18.81	1.900
40	4.39	2.920	8.50	2.595	13.47	2.249	18.13	1.883
60	4.15	2.897	8.08	2.579	12.89	2.237	17.46	1.874
80	3.92	2.883	7.68	2.566	12.34	2.226	16.84	1.862
100	3.70	2.871	7.31	2.554	11.82	2.208	16.24	1.851
130	3.40	2.860	6.78	2.538	11.08	2.200	15.39	1.836
160	3.13	2.844	6.30	2.525	10.39	2.187	14.60	1.823
200	2.80	2.831	5.71	2.508	9.54	2.173	13.60	1.814
240	2.51	2.820	5.18	2.496	8.77	2.162	12.68	1.802
300	2.13	2.802	4.48	2.481	7.73	2.151	11.42	1.790
360	1.80	2.790	3.87	2.470	6.83	2.140	10.33	1.772
k₁×10 min-1	3	2.859	*****	2.538		2.200		1.837
k₂x10 min⁻¹	3 ·	1.325		1.215		1.135	-	1.012
k x10 min-*	3	1.534		1.323		1.065		0.825

.

.

From the above results (Table B - 3), it is seen that when the concentration of $K_2S_2O_{\Theta}$ was increased, there is a decrease in the first order rate constant. It must be mentioned here that in any particular run, (especially that containing high concentration of $K_2S_2O_{\Theta}$) the rate constant slightly decreases with time.

Now in order to study this effect under the condition of constant ionic strength as well as at constant K⁺ ion concentration four kinetic runs having different concentrations of peroxydisulphate and potassium sulphate were studied. The results of these kinetic runs are recorded in Table B - 4 and shown graphically in Fig. B - 2.

It must be mentioned here that, in all the subsequent kinetic studies, though the self decomposition of peroxydisulphate has always been investigated under the corresponding experimental conditions, the kinetic data for these runs have been omitted due to pressure on space and hence only the corresponding values of the rate constant (viz. k_2) have been directly recorded at the end of each table.

$\mu = 0.001$.				
[K ₂ S ₂ O ₀]M + [K ₂ SO ₄]M	0.01 0.09	0.02 0.08,	0.03 0.07	0.04 0.06
Time (min)	Vol. (in n used (viz.	ol) of 0.02 c).	M - Na ₂ S ₂ O	3
0	4.96	9.46	14.36	19.32
20	4.74	9.09	13.88	18.79
40	4.54	8.75	13.44	18.30
60	4.35	8.42	13.01	17.82
80	4.17	8.11	12.60	17.37
100	4.00	7.82	12.21	16.93
130	3.76	7.40	11.65	16.29
160	3.53	7.01	11.13	15.68
200	3.26	6.52	10.46	14.93
240	3.00	6.07	9.87	14.22
300	2.66	5.46	9.01	13.22
360	2.36	4.91	8.24	12.29
k₁ × 10³ min⁻¹	2.120	1.881	1.602	1.309
k₂ × 10³ min⁻¹	0.690	0.670	0.670	0.660
k x 10³ min⁻¹	1.430	1.211	0.932	0.649

AgNO₃ = 1.0 × 10⁻³M, Substrate = 5.0×10^{-2} M, Temp.=35°C. μ = 0.301.

From the results as shown in Table B – 4 it indicates that, here again the first order rate constant is decreased when the concentration of $K_2S_2O_{\Theta}$ was increased.

Table B-5 shows the comparision between k values with the increasing concentrations of peroxydisulphate without K_2SO_4 and with K_2SO_4 to maintain constant ionic strength and constant K+ concentration in the later case.

.

[K ₂ S ₂ O ₀]M without [K ₂ SO ₄] M	kx10 ³ min ⁻¹	[K ₂ S ₂ O ₈]M without constan K* ionic streng	k×10³ stant min ⁻¹ rength	
0.01	1.534	0.01	1.430	
0.02	1.323	0.02	1.211	
0.03	1.065	0.03	0.932	
0.04	0.825	0.04	0.649	

~~~~~

An examination of the above data ,it indicates that at constant K<sup>+</sup> ionic strength , the decrease in the rate constant , with increase in K<sub>2</sub>S<sub>2</sub>O<sub>e</sub> concentration has been minimised .

This suggest that the effect is largely due to the increase in the ionic strength as well as due to the increase in K+ ions concenttration ,both causing inhibition.

There exist a persistent rate decreasing tendancy even though the reaction is carried out at constant ionic strength as well as constant K+ ion concentration.

A plot of -log K versus concentration of peroxydisulphate is found to be linear '(Fig.B-3). The following relationship between -log k and concentration of peroxydisulphate is followed :

- log k = 2.480 + 6.5  $[S_{B}O_{B}^{2-}]_{O} \neq Zero$ . ORDER WITH RESPECT TO PEROXYDISULPHATE

The order with respect to peroxydisulphate was determined by Van't Hoff's<sup>2</sup> differential method. The volume of Na<sub>2</sub>S<sub>2</sub>O<sub>3</sub> (equivalent to K<sub>2</sub>S<sub>2</sub>O<sub>8</sub> was plotted against time for different initial concentration of K<sub>2</sub>S<sub>2</sub>O<sub>8</sub>. From these curves the value of -dc/dt in each case was determined from the initial slope as given in Table B - 6.

| [K <sub>2</sub> S <sub>2</sub> O <sub>6</sub> ]M. | `-dc/dt×10-≁ | Log[ 5 <sub>2</sub> 0 <sub>6</sub> 2-] | Log(-dc/dt) |
|---------------------------------------------------|--------------|----------------------------------------|-------------|
| 0.01                                              | 1.880        | -2.0000                                | -3.7447     |
| 0.02                                              | 3.715        | -1.6990                                | -3.4300     |
| 0.03                                              | 5.643        | -1.5229                                | -3.2484     |
| 0.04                                              | 7.591        | -1.3979                                | -3.1197     |
|                                                   |              |                                        | ×           |

TABLE B - 6

The values of -dc/dt and concentration of [  $S_2O_{e}^{2-}$  are substituted in the Van't Hoff's equation.

 $n = \frac{\log (-dc_1/dt) - \log (-dc_2/dt)}{\log C_1 - \log C_2}$ 

and the order of the reaction is calculated thereby.

The values of (-dc/dt) for different initial concentration of  $S_2 O_{\Theta}^{2-}$  and the value of n calculated there by are recorded in Table B - 7.

| [K28208]M | (-dc/dt) × 10-4 | Order of Reaction(n) |
|-----------|-----------------|----------------------|
| 0.01      | 1.880           | 0.9827               |
| 0.02      | 3.715           |                      |
| 0.01      | 1.880           | 1.0005               |
| 0.03      | 5.643           |                      |
| 0.01      | 1,880           | 1.0066               |
| 0.04      | 7.591           |                      |
| 0.02      | 3.715           | 1.0306               |
| 0.03      | 5.643           |                      |
| 0.03      | 5.643           | 1.0364               |
| 0.04      | 7.591           |                      |

**TABLE B - 7** 

A plot of log (-dc/dt) versus log  $S_2O_{e}^{2-}$  is shown in Fig. B - 4. The slope of the curve is 1.0000 as such the order with respect to  $S_2O_{e}^{2-}$  is one, which is confirmed by the values of n as shown under Table B - 7.

### EFFECT OF SUBSTRATE CONCENTRATION

The effect of amide concentration on the rate of reaction was studied by taking different concentrations of amide. The concentrations of  $S_2O_{\Theta}^{2-}$  and  $AgNO_{3}$  are kept unchanged. Table B - 8 indicates the results of these kinetic ' runs, which have also been represented graphically in Fig.B-5.

| K <sub>2</sub> S <sub>2</sub> O <sub>e</sub> = 2.0 >  | × 10−≃M, AgNO <sub>3</sub> | = 1.0 × 10- | ≫M, Temp.=35                                       | e C.      | •            |
|-------------------------------------------------------|----------------------------|-------------|----------------------------------------------------|-----------|--------------|
| CAmideJM.                                             | 0.025                      | 0.05        | 0.075                                              | 0.1       | 0.125        |
| Time (min)                                            | Vol. (in ml)               | of 0.02 M   | -Na <sub>2</sub> S <sub>2</sub> O <sub>3</sub> use | d (viz. C | )            |
| D                                                     | 9.45                       | 9.44        | 9.46                                               | 9.45      | 9.45         |
| 20                                                    | 8.99                       | 8.95        | 8.97                                               | 8.97      | <b>8.9</b> 6 |
| 40                                                    | 8.56                       | 8.50        | 8.51                                               | 8.53      | 8.50         |
| 60                                                    | 8.15                       | 8.08        | 8.09                                               | 8.11      | 8.07         |
| 80                                                    | 7.77                       | 7.68        | 7.68                                               | 7.71      | 7.66         |
| 100                                                   | 7.41                       | 7.31        | 7.30                                               | 7.35      | 7.28         |
| 130                                                   | 6.90                       | 6.78        | 6.77                                               | 6.82      | 6.75         |
| 160                                                   | 6.43                       | 6.30        | 6.28                                               | 6.34      | 6.25         |
| 200                                                   | 5.85                       | 5.71        | 5.68                                               | 5.75      | 5.65         |
| 240                                                   | 5.34                       | 5.18        | 5.15                                               | 5.22      | 5.12         |
| 300                                                   | 4.64                       | 4.48.       | 4.44                                               | 4.51      | 4.41         |
| 360                                                   | 4.05                       | 3.87        | 3.83                                               | 3.91      | 3.80         |
| k <sub>1</sub> × 10 <sup>3</sup><br>min <sup>-1</sup> | 2.415                      | 2.538       | 2.566                                              | 2.505     | 2.588        |
| k₂x 10³<br>min⁻¹                                      | 1.215                      | 1.215       | 1.215                                              | 1.215     | 1.215        |
| k × 10³<br>min−¹                                      | 1.200                      | 1.323       | 1.351                                              | 1.290     | 1.373        |

From the results of the above table (Table B - 8), it indicates that when the concentration of amide was increased the rate constant remains constant indicating the zero order behaviour of the reaction.

The specific rate is seen to be a function of  $S_2O_{\Theta}^{2-}$  and  $H_2N.OC.CH_2.[CH_2]_5CH_2.CONH_2$  governed by the expression.

 74

ŝ,

In support of the above equation a graph of [Amidelo/k versus concentration of amide is plotted. (Fig. B – 6) and was found to be linear from which  $k_{max}$  and b were evaluated as 0.0030 and 0.03105 respectively. From these values k is calculated and was found to be equal to  $k = 2.485 \times 10^{-3} \text{min}^{-1}$  was almost identical with  $k = 2.538 \times 10^{-3}$  the experimental value.

### ORDER WITH RESPECT TO SUBSTRATE

To confirm the order with respect to substrate the data of Table B - 8 was subjected to Van't Hoff's differential method. From the initial slope of the concentration versus time curves, the value of -dc/dt corrosponding to various initial concentration of substrate were evaluated which are given in Table B - 9.

| [Amide]M. | (-dc/dt) × 10-4 | Log Co  | Log(-dc/dt) |
|-----------|-----------------|---------|-------------|
| 0.025     | 2.719           | -1.6020 | -3.5655     |
| 0.05      | 2.800           | -1.3010 | -3.5528     |
| 0.075     | 2.863           | -1.1249 | -3.5431     |
| 0.10      | 2.748           | -1.0000 | -3.5609     |
| 0.125     | 2.766           | -0.9030 | -3.5581     |

TABLE B - 9

A plot of Log (-dc/dt) versus Log Co is shown in Fig. B - 7, It gives the value of the slope as zero, which suggests that the reaction is zero order with respect to substrate. Calculations were made for the order of the reaction by Van't Hoff's method and are given in Table B-10.

ſ

|               | and also and cost 1994 total state only prov total that total state that they are a state and and and are cost and and |                                                                                                                   |
|---------------|------------------------------------------------------------------------------------------------------------------------|-------------------------------------------------------------------------------------------------------------------|
| [Substrate]M. | (-dc/dt) x 10-4                                                                                                        | Order of Reaction (n)                                                                                             |
| 0.025         | 2.719                                                                                                                  | 0.04232                                                                                                           |
| 0.05          | 2.800                                                                                                                  |                                                                                                                   |
|               |                                                                                                                        |                                                                                                                   |
| 0.025         | 2.719                                                                                                                  | 0.04697                                                                                                           |
| 0.075         | 2.863                                                                                                                  |                                                                                                                   |
|               | ,                                                                                                                      |                                                                                                                   |
| 0.05          | 2.719                                                                                                                  | 0.00765                                                                                                           |
| 0.10          | 2.748                                                                                                                  | ~                                                                                                                 |
|               |                                                                                                                        |                                                                                                                   |
| 0.025         | 2.719                                                                                                                  | 0.01064                                                                                                           |
| 0.125         | 2.766                                                                                                                  | •                                                                                                                 |
|               |                                                                                                                        |                                                                                                                   |
| 0.05          | 2.800                                                                                                                  | 0.05490                                                                                                           |
| 0.075         | 2.863                                                                                                                  |                                                                                                                   |
|               |                                                                                                                        |                                                                                                                   |
| 0.05          | 2.800                                                                                                                  | 0.0133                                                                                                            |
| 0.125         | 2.766                                                                                                                  |                                                                                                                   |
|               | nya man yang pena anya maya paké inin dida laba bina dina dina dina dina dina dina dina d                              | . 1999 and 199 |

This confirms that the order with respect to

- which were stade itself both with which which teach have also which that their advis

substrate is zero.

-----

## EFFECT OF SILVER CATALYST CONCENTRATION

-----

The effect of five different concentrations of silver nitrate on the reaction rate was studied at 35°C. The kinetic data of these runs are recorded in Table B - 11 and shown graphically in Fig. B - 8.

. .

.

TABLE B - 10

| $K_2S_2O_6 = 2.0 \times Temp. = 35^{\circ}C.$      | C <sub>2</sub> S <sub>2</sub> O <sub>0</sub> = 2.0 x 10 <sup>-2</sup> M, Substrate = 5.0 x 10 <sup>-2</sup> M,<br>Temp. = 35°C. |                       |                                       |       |       |  |  |  |
|----------------------------------------------------|---------------------------------------------------------------------------------------------------------------------------------|-----------------------|---------------------------------------|-------|-------|--|--|--|
| [AgNO <sub>3</sub> ]<br>× 10 <sup>-3</sup> M.      | 1.0                                                                                                                             | 1.5                   | 2.0                                   | 3.0   | 4.0   |  |  |  |
| Time (min)                                         | Vol. (in<br>used (vi:                                                                                                           | n ml) of O.<br>z. C). | 02 M - Na <sub>2</sub> S <sub>2</sub> | 03    |       |  |  |  |
| 0                                                  | 9.44                                                                                                                            | 9.45                  | 9.48                                  | 9.46  | 9.44  |  |  |  |
| 20                                                 | 8.95                                                                                                                            | 8.93                  | 8.92                                  | 8.82  | 8.73  |  |  |  |
| 40                                                 | 8.50                                                                                                                            | 8.44                  | 8.41                                  | 8.24  | 8,09  |  |  |  |
| 60                                                 | 8.08                                                                                                                            | 7.99                  | 7.93                                  | 7.70  | 7.50  |  |  |  |
| 80                                                 | 7.68                                                                                                                            | 7.56                  | 7.48                                  | 7.20  | 6.95  |  |  |  |
| 100                                                | 7.31                                                                                                                            | 7.16                  | 7.05                                  | 6.73  | 6.45  |  |  |  |
| 130                                                | 6.78                                                                                                                            | 6.61                  | 6.46                                  | 6.09  | 5.76  |  |  |  |
| 160                                                | 6.30                                                                                                                            | 6.10                  | 5.93                                  | 5.51  | 5.15  |  |  |  |
| 200                                                | 5.71                                                                                                                            | 5.48                  | 5.28                                  | 4.82  | 4.44  |  |  |  |
| 240                                                | 5.18                                                                                                                            | 4.93                  | 4.72                                  | 4.23  | 3.83  |  |  |  |
| 300                                                | 4.48                                                                                                                            | 4.21                  | 3.98                                  | 3.47  | 3.07  |  |  |  |
| 360                                                | 3.87                                                                                                                            | 3.59                  | 3.36                                  | 2.85  | 2.46  |  |  |  |
| k <sub>1</sub> × 10 <sup>3</sup> min <sup>-1</sup> | 2.583                                                                                                                           | 2.747                 | 2.938                                 | 3.386 | 3.792 |  |  |  |

The data(Table B-11) indicates that the specicific rate increases with increasing concentration of silver nitrate. The plot of k versus[Ag+] concentration is found to linear as shown in fig. B-9 and the following relationship is obeyed.

1.442

------

1.560

------

1.514

1.872

------

1.682

2.110

k₂ x 10³min⁻¹ 1.215 1.305 1.378

-----

 $k = 2.1 \times 10^{-3} + 0.4861 [Ag+].$ 

#### EFFECT OF TEMPERATURE

k x 10≊min−₁ 1.323

\_\_\_\_

The reaction was studied at five different tempratures ranging from 25°C to 45°C. The concentrations of all the reactants were kept constant. These kinetic runs are recorded in table B-12 and shown graphically in fig. B -10.

TABLE B - 12

| Temp.                           | 25°C        | 30°C       | 35°C         | 40°C    | 45°C   |
|---------------------------------|-------------|------------|--------------|---------|--------|
| Time(min)                       | Vol.(in ml) | of 0.02M N | la2S203 used | (Viz.C) | 1<br>1 |
| 0                               | 9.46        | 9.46       | 9.44         | 9.42    | 9.44   |
| 20                              | 9.19        | 9.10       | 8.95         | 8.74    | 8.52   |
| 40                              | 8.94        | 8.76       | 8.50         | 8.11    | 7.70   |
| 60                              | 8.71        | 8.44       | 8.08         | 7.53    | 6.96   |
| 80                              | 8.48        | 8.14       | 7.68         | 7.00    | 6.30   |
| 100                             | 8.26        | 7.85       | 7.31         | 6.51    | 5.70   |
| 130                             | 7.95        | 7.44       | 6.78         | 5.84    | 4.91   |
| 160                             | 7.65        | 7.05       | 6.30         | 5.23    | 4.23   |
| 200                             | 7.28        | 6.56       | 5.71         | 4.54    | 3.47   |
| 240                             | 6.93        | 6.13       | 5.18         | 3.93    | 2.85   |
| 300                             | 6.44        | 5.52       | 4.48         | 3.17    | 2.12   |
| 360                             | 5.99        | 4.98       | 3.87         | 2.57    | 1.58   |
| k1 ×10 <sup>3</sup>             | 1.331       | 1.846      | 2.538        | 3.674   | 5.019  |
| k <sub>2</sub> ×10 <sup>3</sup> | 0.670       | 0.820      | 1.215        | 1.618   | 2.505  |
| k ×103                          | 0.661       | 1.026      | 1.323        | 2.056   | 2.514  |

 $K_2S_2O_6=2.0 \times 10^{-2}M$ , Substrate =  $5.0 \times 10^{-2}M$ , AgNO<sub>3</sub>=1.0 ×  $10^{-3}M$ ,

.

The calculated values of (1/T)x10<sup>35</sup> and

log[kr/(kT/h)] are recorded in Table B-13.

# TABLE B -13

| Temp.<br>A° | (1/T)×10 <sup>∞</sup> | krx10³<br>min⁻¹ | log kr  | Log[kr/(kT/h)] |
|-------------|-----------------------|-----------------|---------|----------------|
| 298         | 3.356                 | 0.661           | -4.8202 | -15.9727       |
| 303         | 3.301                 | 1.026           | -3.0111 | -15.7890       |
| 308         | 3.246                 | 1.323           | -3.1216 | -15.6857       |
| 313         | 3.196                 | 2.056           | -3.3131 | -15.5011       |
| 318         | 3.145                 | 2.514           | -3.4004 | -15.4207       |

A plot of log kr versus  $(1/T) \times 10^3$  is found to be linear (Fig. B-11) showing that the reaction obeys Arrhenius relationship.

The energy of activation from the slope of the curve is 12.666 K.cals.mole<sup>-1</sup> which is in good agreement with the calculated value 12.743 K.cals.mole<sup>-1</sup>. Similarly, from the slope of curve obtained by plotting log(kr/(kT/h)) versus  $(1/T)\times10^{3}$  (Fig. B-12) The value of the enthalpy change for the formation of an activated complex  $(\Delta H^{\neq})$  is calculated. The values of E and  $\Delta H^{\neq}$  along with other thermodynamic parameters are recorded in Table B - 14.

| Femp.    kr×10 <sup>3</sup> Temp.    E    A×10 <sup>4</sup> A6 <sup>4</sup> A5 <sup>4</sup> AH <sup>4</sup> A <sup>n</sup> min <sup>-1</sup> coeff.    K.cal.    litre    K.cal.    K.cal.    AH <sup>4</sup> 298    0.661    -    2.487    21.973    -32.78    mole <sup>-1</sup> 298    0.661    -    -    2.487    21.973    -32.78    mole <sup>-1</sup> 203    1.026    2.0015    12.650    2.0109    22.033    -32.654    32.654      308    1.323    2.0038    13.090    1.602    22.233    -32.672    11.842      313    2.054    1.9002    12.743    1.525    22.349    -32.672    11.842      318    2.514    -    1.3203    22.582    -32.912    (Graphica)      ean    -    1.3203    22.584    -32.782    11.842 | Temp.    krx10 <sup>3</sup> Temp.    E    Ax10 <sup>4</sup> A6 <sup>4</sup> A5 <sup>4</sup> A1 <sup>4</sup> A <sup>0</sup> min <sup>-1</sup> coeff.    K.cal.    litre    K.cal.    A      298    0.661    -    -    2.487    21.973    -32.78    mole <sup>-1</sup> 298    0.661    -    -    2.487    21.973    -32.78    mole <sup>-1</sup> 203    1.026    2.0015    12.650    2.0109    21.973    -32.654    *      308    1.323    2.0109    1.602    22.133    -32.657    11.842      313    2.056    1.9002    12.743    1.525    22.345    -32.672    11.842      318    2.514    -    -    1.3203    22.582    -32.912    (Graphica      *ean    -    1.3203    22.582    -32.912    (Graphica | Temp.    kr×10 <sup>3</sup> Temp.    E    A×10 <sup>4</sup> A6 <sup>4</sup> A5 <sup>4</sup> A <sup>n</sup> min <sup>-1</sup> coeff.    K.cal.    litre    K.cal.    a.cal.    e.cal.      298    0.661    -    -    2.487    21.973    -33      298    0.661    -    -    2.487    21.973    -33      203    1.026    2.0015    12.650    2.0109    22.033    -33      308    1.323    2.0038    13.090    1.602    22.033    -33      308    1.323    2.0109    1.602    22.033    -33      313    2.056    1.9002    12.743    1.525    22.349    -33      318    2.514    -    -    1.3203    23.582    -33      318    2.514    -    1.7890    22.5364    -33      4man    -    1.7890    22.3364    -33      4man    -    1.7890    22.3364    -33 | ·                       |                       |                 | TABLE B -             | 14                                       |                             |                | -                                                   |
|-------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|---------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-------------------------|-----------------------|-----------------|-----------------------|------------------------------------------|-----------------------------|----------------|-----------------------------------------------------|
| 298  0.661  -  2.487  21.973  -32.78    503  1.026  2.0015  12.650  2.0109  22.033  -32.654    508  1.323  2.0038  13.090  1.602  22.249  -32.652    513  2.056  1.9002  13.090  1.602  22.345  -32.672  11.842    513  2.054  1.9002  12.743  1.525  22.345  -32.672  11.842    513  2.514  -  -  1.3203  22.582  -32.972  (6raphica)    tean  -  1.9685  12.743  1.525  22.582  -32.972  (6raphica)                                                                                                                                                                                                                                                                                                                         | 298    0.661    -    2.487    21.973    -32.78      303    1.026    2.0015    12.650    2.0109    22.033    -32.654      308    1.323    2.0038    13.090    1.602    22.249    -32.662    11.842      313    2.056    1.9002    12.743    1.525    22.345    -32.672    11.842      318    2.514    -    1.9002    12.743    1.525    22.582    -32.912    (6raphica      318    2.514    -    1.9002    12.743    1.525    22.582    -32.912    (6raphica      318    2.514    -    1.9685    12.743    1.7890    22.5364    +32.782                                                                                                                                                                   | 298    0.661    -    2.487    21.973    -33      303    1.026    2.0015    12.650    2.0109    22.033    -33      308    1.323    2.0038    13.090    1.602    22.249    -33      308    1.323    2.0038    13.090    1.602    22.249    -33      313    2.056    1.902    12.743    1.525    22.345    -33      318    2.514    -    1.3203    22.582    -33      318    2.514    -    1.3203    22.582    -33      318    2.514    -    1.3203    22.582    -33      318    2.514    -    1.3203    22.582    -33      1ean    -    1.9685    12.743    1.7890    22.2364    -33                                                                                                                                                                      | Temp.<br>A <sup>o</sup> | krx10ª<br>ain a       | Temp.<br>coeff. | E<br>K.cal.<br>mole-1 | Ax104<br>litre<br>mole- <sup>1</sup> sec | ∆6★<br>K.cal.<br>:-1 mole-* | ▲34<br>Pe- Li. | ∆H <del>+</del><br>K.cal<br>mole-1                  |
| 303  1.026  2.0015  12.650  2.0109  22.033  -32.654    508  1.323  2.0038  13.090  1.602  22.249  -32.1862    513  2.056  1.9002  12.743  1.525  22.345  -32.672  11.842    518  2.514  -  1.3203  22.582  -32.942  (Graphica)    518  2.514  -  1.3203  22.582  -32.942  (Graphica)    518  2.514  -  1.9665  12.743  1.525  22.544  -32.942  (Graphica)    fean  -  1.9665  12.743  1.7890  22.2564  -32.782  -32.782                                                                                                                                                                                                                                                                                                       | 303    1.026    2.0015    12.650    2.0109    22.033    -32.654      308    1.323    2.0038    13.090    1.602    22.249    -321862      313    2.056    1.9002    12.743    1.525    22.345    -32.672    11.842      313    2.056    1.9002    12.743    1.525    22.345    -32.672    11.842      318    2.514    -    -    1.3203    22.582    -32.942    (Graphicater detain)      318    2.514    -    -    1.3203    22.582    -32.942    (Graphicater detain)      318    2.514    -    -    1.3203    22.582    -32.942    (Graphicater detain)      1ean    -    1.9685    12.743    1.7890    22.2364    -32.782    -                                                                         | 303    1.026    2.0015    12.650    2.0109    22.033    -33      308    1.323    2.0038    13.090    1.602    22.249    -33      313    2.056    1.9002    12.743    1.525    22.345    -33      318    2.514    -    1.525    22.345    -33      318    2.514    -    1.3203    22.582    -33      318    2.514    -    1.3203    22.582    -33      318    2.514    -    1.3203    22.564    -33      4ean    -    1.9685    12.743    1.7890    22.2364    -33                                                                                                                                                                                                                                                                                       | 298                     | 0.661                 |                 |                       | 2.487                                    | 21.973                      | -32.78         | A 1977 1985 1997 1998 1998 1998 1998 1998 1998 1998 |
| 508  1.323  2.0038  13.090  1.602  22.249  -32.862    513  2.056  1.9002  12.743  1.525  22.345  -32.672  11.842    518  2.514  -  1.3203  22.582  -32.912  (6raphica)    518  2.514  -  1.3203  22.582  -32.912  (6raphica)    518  2.514  -  1.9685  12.743  1.7890  22.2564  -32.782                                                                                                                                                                                                                                                                                                                                                                                                                                       | 308  1.323  2.0038  13.090  1.602  22.249  -32(862    313  2.056  1.9002  12.743  1.525  22.345  -32.672  11.842    318  2.514  -  -  1.3203  22.582  -32.942  (Graphice    318  2.514  -  -  1.3203  22.582  -32.942  (Graphice    1  1.9685  12.743  1.7890  22.2364  -32.782                                                                                                                                                                                                                                                                                                                                                                                                                          | 308    1.323    2.0038    13.090    1.602    22.249    -33      313    2.056    1.9002    12.743    1.525    22.345    -33      318    2.514    -    -    1.3203    22.582    -33      318    2.514    -    1.3203    22.582    -33      ifean    -    1.9685    12.743    1.7890    22.2364    -33                                                                                                                                                                                                                                                                                                                                                                                                                                                     | 203                     | 1.026                 | 2.0015          | 12.650                | 2.0109                                   | 22.033                      | -32.654        | ·<br>·                                              |
| 513  2.056  1.9002  12.743  1.525  22.345  -32.672  11.842    518  2.514  -  -  1.3203  22.582  -32.942  (Graphica)    -  -  1.3203  22.5364  -32.782  -32.782    tean  -  1.9685  12.743  1.7890  22.2364  -32.782                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | 513  2.056  1.9002  12.743  1.525  22.345  -32.672  11.842    518  2.514  -  -  1.3203  22.582  -32.942  (Graphication)    51  -  -  1.3203  22.582  -32.942  (Graphication)    1  -  -  1.9685  12.743  1.7890  22.2364  -32.782                                                                                                                                                                                                                                                                                                                                                                                                                                                                        | 513    2.056    1.9002    12.743    1.525    22.345    -33      518    2.514    -    -    1.3203    22.582    -33      7    -    -    1.3203    22.582    -33      1    -    -    1.3203    22.582    -33      1    -    -    1.3203    22.582    -33      1    -    -    1.9685    12.743    1.7890    22.2364    -33      1    -    1.7890    22.2364    -33                                                                                                                                                                                                                                                                                                                                                                                          | 308                     | 1.323                 | 2.0038          | 13.090                | 1.602                                    | 22.249                      | -321862        |                                                     |
| S18  2.514  -  1.3203  22.582  -32.942  (Braphica)                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            | 318 2.514 - 1.3203 22.582 -32.912 (Graphica<br>1.1.9685 12.743 1.7890 22.2364 -32.782                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    | 318 2.514 - 1.3203 22.582 -33                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | 213                     | . 2.056               | 1.9002          | 12,743                | 1.525                                    | 22 - 345                    | -32.672        | 11.842                                              |
| tean - 1.9685 12.743 1.7890 22.2364 +32.782                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   | 1.7890 22.2364 -32.782                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   | lean - 1.9685 12.743 1.7890 22.2364 -32                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 | 518<br>                 | 2.514                 | 1               | i                     | 1.3203                                   | 22.582                      | -32.942        | (Graphica))                                         |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         | tean                    | 1<br>1<br>1<br>1<br>1 | 1.9685          | 12.743                | 1.7890                                   | 22.2364                     | -32.782        |                                                     |

• •

-

i

. .

·

,

80 . .

.

•

A large negative value of entropy of activation is indicative of the formation of an activated complex involving either two oppositely charged ions or an ion and a neutral molecule.

The rate constant for this reaction may be expressed by the following relation.  $\stackrel{\prime}{,}$ 

k = 1.7890 . e<sup>-12.743/RT</sup> sec<sup>-1</sup>

# EFFECT OF IONIC STRENGTH :

The effect of varying ionic strength on the reaction rate was studied by adding different amounts of  $K_2SO_4$  to the reaction mixture. The results of these kinetic runs are recorded in Table B - 15 and shown graphically in Fig. B-13.

|                                          | 1.0 ×10-3    | 1, Temp = 35  | 5°C.        | · · · ·       |               |               |
|------------------------------------------|--------------|---------------|-------------|---------------|---------------|---------------|
| K <b>₂SO₄M</b><br>u                      | NIL<br>0.061 | 0.01<br>0.091 | 0.015       | 0.02<br>0.121 | 0.03<br>0.151 | 0.04<br>0.181 |
| Time(mi                                  | n) Vol. (    | (in ml.) of   | f 0.02 M Na | 25203 used    | (viz.C)       |               |
| ο                                        | .9.44        | 9.45          | 9.48        | 9.45          | 9.48          | 9.45          |
| 20                                       | 8.95         | 9.02          | 9.11        | 9.10          | 9.16          | 9.12          |
| 40                                       | 8.50         | 8.62          | 8.76        | 8.77          | 8.86          | 8.80          |
| 60                                       | 8.08         | 8.25          | 8.43        | 8.46          | 8.57          | 8.51          |
| 80                                       | 7.68         | 7.89          | 8.11        | 8.16          | 8.29          | 8.22          |
| 100                                      | 7.31         | 7.55          | 7.81        | 7.88          | 8.03          | 7.95          |
| 130                                      | 6.78         | 7.08          | 7.39        | 7.48          | 7.65          | 7.56          |
| 160                                      | 6.30         | 6.63          | 6.99        | 7.10          | 7.30          | 7.20          |
| 200                                      | 5.71         | 6.08          | 6.49        | 6.63          | 6.86          | 6.74          |
| 240                                      | 5.18         | 5.58          | 6.03        | 6.19          | 6.44          | 6.32          |
| 300                                      | 4.48         | 4.91          | , 5.41      | 5.59          | 5.88          | 5.74          |
| 360                                      | 3.87         | 4.33          | 4.86        | 5.06          | 5.36          | 5.22          |
| k₁×10 <sup>33</sup><br>min <sup>−1</sup> | 2.538        | 2.225         | 1.915       | 1.794         | 1.640         | 1.708         |
| k₂×10³<br>min⁻¹                          | 1.215        | 1.120         | 0.980       | 0.930         | 0.800         | 0.780         |
| k ×10³<br>min⁻¹                          | 1.323        | 1.105         | 0.935       | 0.864         | 0.840         | 0.928         |

substrates 0 v10-2M V 0 0 -2 0 -10-2M

From the results given in Table B - 15 it indicates that the salt effect is negative.

On plotting log k against  $u^{1/2}$  as well as k against u as shown in Fig. 14 (A) and 14(B) respectively, it is found that log k versus  $u^{1/2}$  curve is linear in the region of low ionic strength ( < 0.2 ), while there exists no linearity in the plot k versus u . This suggests that the salt effect is at primary exponential type

in the region of low ionic strength indicating that the rate determining process involves a reaction between two oppositely charged ions.

 $k \times 10^3 \min^{-1} \sqrt{\mu}$  Log k [K2SO4]M μ 1.323 0.061 Nil 0.247 -2.8784 1.105 0.01 0.091 0.302 -2.9566 0.935 0.015 0.106 0.326 -3.0292 0.864 0.02 0.121 0.348 -3.0635 0.03 0.151 0.840 0.389 -3.0757 0.04 0.181 0.928 0.425 -3.0325 

TABLE B - 16

It may be stated that the ionic strength employed is rather high for Bronsted relationship to be strictly applicable quantitatively, but still the agreement is found to be fairly good.

### SPECIFIC IONIC EFFECT

The following table (Table B-17 ) includes the result of the kinetic runs investigating the effect of vrious cations on the rate of this reaction. These data have also been shown graphically in Fig. B-15. This study has been carried out at constant ionic strength.

| Т | A | B | L | Ε  | В   |             | 17          |  |
|---|---|---|---|----|-----|-------------|-------------|--|
| ~ | ~ | ~ | ~ | ~~ | ~~~ | $\sim \sim$ | $\sim \sim$ |  |

| K <sub>2</sub> S <sub>2</sub> O <sub>8</sub> = 2<br>AgNO <sub>3</sub> = 1.0 | .0 × 10<br>× 10-3 | −² M, Su<br>M, Temp. | bstrate =<br>= 35°C, | 5.0 × 10-<br>u = 0.212                          | -2M,<br>?   |        |
|-----------------------------------------------------------------------------|-------------------|----------------------|----------------------|-------------------------------------------------|-------------|--------|
| Salt<br>added                                                               | No<br>Salt        | K₂\$0₄               | Na <sub>2</sub> SO4  | Li <sub>2</sub> SO <sub>4</sub>                 | MgSO₄       | ZnSO4  |
| (conc.)M                                                                    | 0.00              | 0.05                 | 0.05                 | 0.05                                            | 0.0375      | 0.0375 |
| Time(min)                                                                   | Vol. (            | in ml.)              | of 0.02 M            | Na <sub>2</sub> S <sub>2</sub> O <sub>3</sub> L | used(viz.C) |        |
| 0                                                                           | 9.44              | 9.48                 | 9.46                 | 9.45                                            | 9.48        | 9.45   |
| 20                                                                          | 8.95              | 9.20                 | 9.11                 | 9.07                                            | 9.07        | 9.01   |
| 40                                                                          | 8.50              | 8.94                 | 8.79                 | 8.71                                            | 8.69        | 8.61   |
| 60                                                                          | 8.08              | 8.69                 | 8.48                 | 8.37                                            | 8.32        | 8.22   |
| 80                                                                          | 7.68              | 8.45                 | 8.18                 | 8.04                                            | 7.98        | 7.86   |
| 100                                                                         | 7.31              | 8.22                 | 7.90                 | 7.73                                            | 7.65        | 7.52   |
| 130                                                                         | 6.78              | 7.89                 | 7.50                 | 7.30                                            | 7.19        | 7.03   |
| 160                                                                         | 6.30              | 7.58                 | 7.13                 | 6.88                                            | 6.76        | 6.58   |
| 200                                                                         | 5.71              | 7.19                 | 6.66                 | 6.38                                            | 6.23        | 6.02   |
| 240                                                                         | 5.18              | 6.82                 | 6.23                 | 5.91                                            | 5.74        | 5.52   |
| 300                                                                         | 4.48              | 6.30                 | 5.64                 | 5.28                                            | 5.09        | 4.84   |
| 360                                                                         | 3.87              | 5.83                 | 5.10                 | 4.72                                            | 4.51        | 4.26   |
| k₁×10³<br>min⁻¹                                                             | 2.538             | 1.405                | 1.776                | 1.987                                           | 2.122       | 2.270  |
| k₂×10³<br>min−¹                                                             | 1.215             | 0.770                | 0.943                | 0.860                                           | 0.880       | 0.980  |
| k ×10³<br>min−¹                                                             | 1.323             | 0.635                | 0.733                | 1.127                                           | 1.242       | 1.290  |

It is seen that the specific inhibitory effect of the various ions is in the order.

 $K^+$  > Na<sup>+</sup> > Li<sup>+</sup> > Mg<sup>2+</sup> > Zn<sup>2+</sup>

# EFFECT OF HYDROGEN ION CONCENTRATION

The solution of substrate was prepared in 10% acetic acid, and hence it is not possible to study the effect of acid, such as sulphuric acid on the reaction rate.

### EFFECT OF ALLYL ACETATE

. .....

The reaction was carried out in the absence of and at three different initial conentrations of allyl acetate. The results of these kinetic runs are summarised in Table B-18 and shown graphically in Fig. B-16.

#### TABLE B - 18

| K2S2(<br>AgNO;    | ) <sub>æ</sub> = 2.0 ×<br>s = 1.0 × 10                  | 10 <sup>-2</sup> M, subst<br>- <sup>3</sup> M, Temp. | rate = 5.0 ;<br>= 35°C. | < 10-2 M,                                |       |
|-------------------|---------------------------------------------------------|------------------------------------------------------|-------------------------|------------------------------------------|-------|
| Allyl             | Acetate                                                 | Nil                                                  | 0.001                   | 0.005                                    | 0.01  |
| Time              | (min)                                                   | Vol. (in<br>used(viz. C                              | ml.) of ()<br>)         | .02M - Na <sub>2</sub> S <sub>2</sub> O; | 3     |
| 0                 | 147 bibs will the same the time and and and and and and | 9.44                                                 | 9.45                    | 9.48                                     | 9.46  |
| 20                |                                                         | 8.95                                                 | 9.00                    | 9.08                                     | 9.10  |
| 40                |                                                         | 8.50                                                 | 8.58                    | 8.71                                     | 8.76  |
| 60                |                                                         | 8.08                                                 | 8.19                    | . 8.36                                   | 8.45  |
| 80                |                                                         | 7.68                                                 | 7.82                    | 8.02                                     | 8.14  |
| 100               |                                                         | 7.31                                                 | 7.46                    | 7.70                                     | 7.85  |
| 130               |                                                         | 6.78                                                 | 6.96                    | 7.52                                     | 7.44  |
| 160               |                                                         | 6.30                                                 | 6.50                    | 6.82                                     | 7.05  |
| 200               |                                                         | 5.71                                                 | 5.93                    | 6.30                                     | 6.57  |
| 240               |                                                         | 5.18                                                 | 5.42                    | 5.81                                     | 6.12  |
| 300               |                                                         | 4.48                                                 | 4.74                    | 5.17                                     | 5.51  |
| 360               |                                                         | 3.87                                                 | 4.14                    | 4.59                                     | 4.96  |
| 10 <sup>3</sup> ( | nin-1                                                   | 2.538                                                | 2.345                   | 2.062                                    | 1.843 |

From the data contained in Table 8-18, indicates that allyl acetate inhibits the rate of reaction. So the reaction involving  $S_2 O_{e^2}$  are greatly inhibited by allyl acetate which acts as a sulphate radical trapping reagent. The radical trapping may be due to the polymerisation of allyl acetate by sulphate ions formed from the catalysed decomposition of peroxydisulphate ion .

# MOLE RATIO

For determining mole ratio between  $K_2S_2O_8$  and amide, two kinetic runs were carried out simultaneously, one in the presence of amide and the other in the absence of amide. In both the kinetic runs the concentration of  $K_2S_2O_8$ was the same and was five times than the concentration of amide. The concentration of the catalyst was the same in both the runs. At suitable intervals of time 5 ml. of the reaction mixture was pipetted out and estimated for unreacted  $S_2O_8^{2-}$ . These results are recorded in Table B - 19 and shown graphically in Fig. B - 17.

|       |       |                     | ••••••••••••••••••••••••••••••••••••••                         |   |
|-------|-------|---------------------|----------------------------------------------------------------|---|
| Subst | rate  | 0.01                | Nil                                                            |   |
| Time  | (min) | Vol.(in ml) of 0.03 | 2 M -Na <sub>2</sub> S <sub>2</sub> O <sub>3</sub> used (vizC) |   |
| O     |       | 24.34               | 24.95                                                          |   |
| 30    |       | 21.07               | 23.38                                                          |   |
| 60    |       | 21.21               | 23.33                                                          |   |
| 90    |       | 19.78               | 21.41                                                          |   |
| 120   |       | 18.50               | 20.82                                                          |   |
| 150   |       | 17.41               | 20.37                                                          |   |
| 180   |       | 16.28               | 19.46                                                          | • |
| 210   |       | 15.03               | 19.01                                                          |   |
| 240   |       | 13.76               | 18.16                                                          |   |
| 270   |       | 13.08               | 17.33                                                          |   |
| 300   |       | 12.17               | 16.92                                                          |   |
| 330   |       | 11.61               | 15.84                                                          |   |
| 360   |       | 10.86               | 15.81                                                          |   |
| 390   |       | 10.78               | 15.02                                                          |   |
| 420   |       | 10.48               | 14.42                                                          |   |
| 450   |       | 9.94                | 13.96                                                          |   |
| 480   |       | 9.52                | 13.47                                                          | ł |
|       |       |                     |                                                                |   |

K<sub>2</sub>S<sub>2</sub>O<sub>8</sub> = 5.0 × 10<sup>-2</sup>M, AgNO<sub>3</sub>= 1.0× 10<sup>-3</sup>M, Temp.= 35°C

The curve (Fig. B-17) consists of two portions, the first for the oxidation of amide and second for self decomposition of peroxydisulphate ion. Now tangents are drawn at portion of the curve which intersect at point P. From this point of intersection the value of  $K_2S_2O_8$  consumed in the complete oxidation of 10 ml of 0.01 amide is calculated. The point Q on the curve at the same time gives the value corresponding to self decomposition of  $K_2S_2O_8$ . From the graph (Fig. B - 17) it indicates that the two plots become parallel at P. At this point log C = 1.1 which corresponds to 12.58 ml.

The corresponding value of log C at the same time on the self decomposition curve is shown by point Q. At this point log C = 1.23 which corresponds to 16.98 ml.

> The difference between the two values is 4.4 ccs. Therefore, 4.4 ccs of

 $0.02 \text{ N} \text{ Na}_2\text{S}_2\text{O}_3 = 4.4 \text{ ccs} \text{ of } 0.02 \text{ N} \text{ K}_2\text{S}_2\text{O}_8$ 

= 4.4 ccs of 0.01N .K2S20

Hence 10 ml of 0.01 M amide = 4.4 ml. of 0.01  $K_2S_2O_e$  Thus one mole of amide consumes one mole of peroxydisulphate for completion of the reaction.



FIG. B-1 EFFECT OF K2S208



FIG - B - 2

OF K2S208 AT CONSTANT 4



FIG. B-3 PLOT OF LOG K VS CONC. OF K2S208

,









FIG B-6 PLOT OF AMIDE / k VS k





FIG. B-8 PLOT OF LOG C VS TIME



.

.



EFFECT OF



FIG. B-11 PLOT OF LOG k VS 1/T x 10<sup>3</sup>















